# **GATE**2019

# ELECTRICAL MACHINE

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### A Unit of ENGINEERS CAREER GROUP

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**GATE-2019:** Electrical Machine| Detailed theory with GATE & ESE previous year papers and detailed solu ons.

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### CHAPTER - 1 TRANSFORMERS

### **1.1 PHASOR DIAGRAMS**



### Phasor Diagram of vector A

Phasor rotating vector

**1.** If all vectors are rotating at same frequency then only phase difference and amplitude of vector is to be known for vector operation.

2. Angle measured in counter clock- wise (ccw) direction are positive.

3. Angle measured in clock wise (cw) directions are negative.

4. If  $\vec{R}_1$  is taken as reference then angle of  $\vec{R}_1$  is Zero (0°).  $\vec{R}_2$  vector is ahead or leading  $\vec{R}_1$  by

 $\theta_2^{\circ}$  and vector  $\vec{R}_3$  is lagging  $\vec{R}_1$  by  $\theta_3^{\circ}$ . And the vector  $R_1 R_2$  and  $R_3$  will be represented as :



- $R_1 \angle 0^\circ, R_2 \angle \theta_2^\circ \text{ and } R_3 \angle -\theta_3^\circ$
- 5. In phasor form always RMS values of amplitudes are taken.
- 6. Adding or subtracting vectors.
- Let  $\vec{R} = \vec{R}_1 + \vec{R}_2$  is to be find out.
- I. Place or draw  $\vec{R}_1$



II. At the end of  $\vec{R}_1$ ,  $\vec{R}_2$  will have its beginning end, and hence join the ends of  $R_1$  and  $R_2$  as:



7.  $|\mathbf{R}| \ge \theta$  is represented on axis as the length of OB is equal to magnitude of  $\mathbf{\vec{R}} = |\mathbf{R}|$ 

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# GATE QUESTIONS

1. A three – phase, three winding  $\Delta/\Delta/Y$  (1.1 kV/6.6kV/400V) transformer is energized from (a) 22 AC mains at the 1.1 kV side. It Supplies 900 kVA load at 0.8 power factor lag from the 6.6 kV winding and 300 kVA load at 0.6 power factor lag from the 400V winding. The RMS line current in ampere drawn by the 1.1 kV winding from the mains is \_\_\_\_.

### [GATE - 2017]

**2.** If the primary line voltage rating is 3.3 kV(Y side) of a 25 kVA, Y- $\Delta$  transformer (the per phase turns ratio is 5;1), then the line current rating of the secondary side (in Ampere) is

[GATE - 2017]

**3.** If an ideal transformer has an inductive load element at port 2 as shown in the figure below, the equivalent inductance at port 1 is



**4.** A single phase 400V, 50Hz transformer has no iron loss of 5000 W at the rated condition. When operated at 200V, 25Hz, the iron loss is 2000 W. when operated at 416V, 52Hz the value of the hysteresis loss divided by the eddy current loss is

### [GATE - 2016]

**5.** A single – phase 22kVA, 220 V/220V, 50Hz, distribution transformer is to be connected as an auto transformer to get an output voltage of 2420V. Its maximum kVA rating as an auto- transformer is

[GATE - 2016] (b) 24.2 (d) 2420

A

**6.** A single phase 2 kVA, 100/200 V transformer is reconnects as an auto – transformer such that its kVA rating is maximum. The new rating, in kVA, is

### [GATE - 2016]

7. Three single phase transformers are connected to form a delta – star three - phase transformer of 110 kV/11kV. The transformer supplies at 11 kV a load of 8 MW at 0.8p.f lagging to a nearby plant. Neglect the transformer losses. The ratio phase currents in delta side to star side is

	[GATE - 2016]
(a) $1:10\sqrt{3}$	(b) $10\sqrt{3}:1$
(c) 1 : 10	(d) $\sqrt{3}:1$

**8.** For a specified input voltage and frequency, if the equivalent radius of the core of a transformer is reduced by half, the factor by which the number of turns in the primary should change to maintain the same no load current is

	[GATE - 2014]
(a) 1/4	(b) 1/2
(c) 2	(d) 4

**9.** The core loss of a single phase, 230/115V, 50Hz power transformer is measured from 230 V side by feeding the primary (230 V side) from a variable voltage variable frequency source while keeping the secondary open circuit. The core loss is measured to be 1050 W for 230 V, 50 Hz input. The core loss is again measured to be 500W for 138 V, 30 Hz input. The hysteresis and eddy current losses of the transformer for 230 V, 50 Hz input are respectively.



### CHAPTER - 2 BASICS OF ENERGY CONVERSION & ROTATING MACHINES

### **2.1 INTRODUTION**

For conversion of energy from electrical to mechanical and mechanical to electrical, there must be coupling field, the coupling field must react in such a way that over all conversion draws energy from source and deliver to load.



$$\begin{split} W_{elect} &= W_{fld} + W_{mech.} \\ dW_{elect} &= dW_{fld} + dW_{mech.} \end{split}$$

### **2.2 COUPLING FIELD**

Coupling field is the link between electrical and mechanical system and energy stored in coupling field produces action and reaction on electrical and mechanical system.

This Coupling field may be magnetic or electrostatic field, but capacity of magnetic field to store energy is 25000 times more than electrostatic energy. Thus, magnetic field is used as coupling field.

Electrical input = e i dt

$$dW_{elec.} = i.e.dt \left| \because e = \frac{d\psi}{dt} \Longrightarrow edt = d\psi \right|$$

 $dW_{elec.} = id\psi$ 

Where  $\psi$  is flux linkage

 $\psi = Li = N\phi$ 

 $\Rightarrow d w_{elec} = I d(N \phi) = iNd\phi$  $\Rightarrow d W_{elec} = F d\phi$ 

Where F is magnetomotive force

### 2.3 MAGNETIC FIELD ENERGY STORED









### **3.1 BASIC STRUCTURE OF ELECTRIC MACHINE**

- 1. Stator: Stationary part and normally is the outer frame of the machine.
- 2. Rotor: Rotating part and generally inner part of the machine.
- 3. Armature Winding: The winding in which voltage is induced.
- 4. Field Winding: The winding through which a current is passed to produce the main flux.

### **3.2 TYPES OF D.C MACHINE**

- 1. D.C Generator: It convert mechanical energy into electrical energy.
- 2. D.C Motor: It converts electrical energy into mechanical energy.

### **3.3 D.C MACHINE CONSTRUCTION**

- D.C. Machine consists of three main parts:
- 1. Magnetic field system
- 2. Armature
- 3. Commutator and brush gear.

### 1. Magnetic Field System

(i) It is the fixed or stationary part of the machine.

(ii) It produces the main magnetic flux.

(iii) The field winding is placed on poles, projected inward and hence they are called salient poles with poles with pole shoes.

- (iv) Pole shoe serve two purposes:-
- (a) It supports the field coils

(b) It increase the cross – sectional area of magnetic circuit and hence  $R_e$  decreases



Main part of the 4.pole DC. Machine



1. A separately excited DC generator supplies while running at 600 rpm. 150A to a 145 VDC grid. The generator is running at 800 RPM. The armature resistance of in an armature conductor of the motor is given the generator is  $0.1\Omega$ . If the speed of the by generator is increased to 1000 RPM, the current in amperes supplied by the generator to the DC grid is

[GATE - 2017] (a)

2. A 220V DC series motor runs drawing a current of 30A fro mthe supply. Armature and field circuit resistances are  $0.4\Omega$  and  $0.1\Omega$ , respectively. The load torque varies as the square of the speed. The flux in the motor may be taken as being proportional to the armature current. To reduce the speed of the motor by 50% the resistance in ohms that should eb added in series with the armagure is . (Given the answer up to two decimal places)

[GATE - 2017]

3. A 120 V DC shunt motor takes 2 A at no load. It takes 7A on full load while running at 1200 rpm. The armauture resistance is  $0.8\Omega$  and the shunt field resistance is  $240\Omega$ . The no load speed, in rpm, is

4. A 220V, 10 kW, 900 rpm separately excited DC motor has an armature resistance  $R_a =$  $0.02\Omega$ . When the motor operates at rated speed and with rated terminal voltage, the electromagnetic torque developed by the motor is 70Nm. Neglecting the rotational losses of the machine, the current drawn by the motor from the 220V supply is

5. A 4-pole, lap - connected separately excited dc motor is drawing a steady current of 40A

А good approximation for the waveshape of the current



6. A DC shunt generator delivers 45 A at a terminal voltage of 220 V. The armature and the shunt field resistances are  $0.01\Omega$  and  $44\Omega$ respectively. The stray losses are 375 W. the percentage efficiency of the DC generator is

### [GATE - 2016]

7. A three-phase, 50Hz salient-pole synchronous motor has a per - phase directaxis reactance (X<sub>d</sub>) of 0.8 pu and a per phase

### **CHAPTER - 4** SYNCHRONOUS MACHINE

### **4.1 INTRODUCTION**

### 4.1.1 Construction and Working Principle

A synchronous machine essentially consists of two parts.

1. Armature (Rotor)

2. Field Magnet System

An alternation may be constructed with either the armature or the field structure as the revolving system. Stator is the stationary part of the machine it carries the armature winding in which the voltage is generated and hence output is taken from stator. The rotor is the rotating part of the machine. The rotor produces the main field flux.

### **1.** Stator Construction

It includes the frame, stator core, stator windings and cooling arrangement, where frame may be of cast iron for small size machines.



### 2. Rotor Construction

There are two types of rotor constructions namely salient-pole type and cylindrical rotor type.

### **4.2 SALIENT POLE TYPE**

Consists of poles projecting out from the surface of rotor core. Salient pole rotors are normally used for rotors with four or more poles.



### 4.2.1 Six Pole Salient Pole Rotor

Salient pole rotors have concentrated winding on the poles. And it has generally non-uniform air gap. And hence pole phases are so formed that this non-uniform flux becomes sinusodially which

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GATE QUESTIONS

1. Two parallel connected, three - phase, 50Hz, 11kV, star - connected synchronous machines A and B, are operating as synchronous condensers. They together supply 50MVAR to a 11kV grid. Current supplied by both the machines are equal. Synchronous reactance's of machine A and machine B are 1 $\Omega$  and 3 $\Omega$ , respectively. Assuming the magnetic circuit to be linear, the ratio of excitation current of m machine A to that of machine B is \_\_\_\_\_.(given the answer up to two decimal places).

### [GATE - 2017]

**2.** A three - phase, 50hz, star - connected cylindrical - rotor synchronous machine is running as a motor. The machine is operated from a 6.6kV grid and draws current at unity power factor (UPF). The synchronous reactance of the motor is  $30\Omega$  per phase. The load angle is  $30^{\circ}$ . The power delivered to the motor in kW is

\_\_\_\_\_ (Give the answer up to one decimal place)

[GATE - 2017]

**3.** Two generating units rated 300MW and 400MW have governor speed regulation of 6% and 4% respectively from no load to full load. Both the generating units are operating in parallel to share a load of 600MW. Assuming free governor action, the load shared by the larger units is \_\_\_\_\_ MW.

[GATE - 2017]

4. A 25 kVA, 400V,  $\Delta$  - connected, 3-phase, cylindrical rotor synchronous generator requires a field current of 5A to maintain the rated armature current under short – circuit condition. For the same field current, the open – circuit voltage is 360V. Neglecting the armature resistance and magnetic saturation, its voltage regulation (in % with respect to terminal voltage), when the generator delivers the rated

1. Two parallel connected, three - phase, 50Hz, load at 0.8 pf leading at rated terminal voltage is

G

### [GATE - 2017]

**5.** A 3-phase, 2-pole, 50hz, synchronous generator has a rating of 250 MVA, 0.8 pf lagging. The kinetic energy of the machine at synchronous speed is 100MJ. The machine is running steadily at synchronous speed and delivering 60MW power at a power angle of 10 electrical degrees. If the load is suddenly removed, assuming the acceleration is constant for 10 cycles, the value of the power angle after 5 cycles is electrical degrees.

[GATE - 2017]

**6.** A star connected 400 V, 50 Hz, 4 pole synchronous machine gave the following open circuit and short circuit test results;'

Open circuit test :  $V_{\alpha} = 400V$  (rms, line -to - line) at field current,

 $I_f = 2.3 \text{ A}$ 

Short circuit test:  $I_{sc} = 10$  A (rms, phase) at field current.

 $I_{f} = 1.5 A$ 

The value of per phase synchronous impedance in  $\Omega$  at rated voltage is  $\Omega$ .

[GATE - 2014]

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7. A three phase synchronous generator is to be connected to the infinite bus. The lamps are connected as shown in the figure for the synchronization. The phase sequence fo bus voltage is R-Y-B and that of incoming generator voltage is R' - Y' - B'.

## 

### CHAPTER - 5 INDUCTION MOTOR

### **5.1 INTRODUCTION**

**5.1.1 Stator Emf** In general emf induced in coil  $E = K_w N_{phs} \phi_p \omega_r \sin(\omega_r t - \pi/2)$ E is Induced emf

 $K_w$  is Winding factor  $N_{phs}$  is Number of seires turns per phase

 $\phi_p$  is Flux per pole

 $\omega_r$  is Relative angular velocity

 $Sin(\omega_r t - \pi/2)$ 

: Induced emf in stator

 $E_s = K_{ws} N_{phs} \phi_p \omega_s$ 

Induced emf in rotor, at stand still

 $E_r = K_{ws} N_{phr} \phi_p \omega_r$ 

Instantaneous emf induced in rotor

$$K_{wr} N_{phs} \phi(\omega_s - \omega_r) sin[(\omega_s - \omega_r)t - \pi/2]$$

Rotating field rotates at synchronous speed cuts the rotor bar conductors which generates emf and as rotor conductors are short circuited hence current will flow in it, which produces its own emf and interaction of these two emf. produces torque. As per Lenzes Law, the effect opposes the cause, here effect is rotation of rotor and causes is relative velocity between fields.

· Rotor rotates in direction as to decrease the relative velocity.

$$\omega_s$$
 -  $\omega_r$  is slip speed

Where relative velocity = slip speed,

$$S(slip) = \frac{\omega_s - \omega_r}{\omega_s} = \frac{N_s - N_r}{N_s} = \frac{\text{Relative speed}}{\text{Synchronous speed}}$$

 $N_r = (1 - S) N_s$ 

 $= K_{wr} N_{phs} \phi S \omega_s \sin [t - \pi/2]$ 

 $\therefore$  Frequency and amplitude of rotor emp. Both becomes S-times the stator amplitude and frequency.

If (At stand still), S = 1,  $E_r = E_2$ ,  $f_r = f_2$  then at any slip say S,  $E_r = SE_2$ ,  $f_r = Sf_2$ 

### 5.2 CONSTRUCTIONAL FEATURES

### 5.2.1 Stator

Frame made-up of cost iron. Stator core made-up of laminated steel i.e., bearing, slip ring and shaft. 3– phase uniformly distributed winding electrically spread 120°.



induction generator. The generator supply operating at a speed of 700 rpm. The frequency frequency is 60Hz. The rotor current frequency is 5Hz. The mechanical speed of the rotor in RPM is

	[GATE - 2017]
(a) 1350	(b) 1650
(c) 1950	(d) 2250

2. A 3-phase, 50Hz generator supplies power of 3MW at 17.32 kV to a balanced 3-phae inductive load through an overhead line. The per phase line resistance and reactacne are  $0.25\Omega$  and  $3.925\Omega$  respectively. If the voltage at the generator terminal is 17.87 kV, the power factor of the load is

[GATE - 2017] 3. A star - connected, 12.5 kW, 208V (line), 3phase, 60hz squirrel cage induction motor has following equivalent circuit parameters per phase referred to the stator.  $R_1 = 0.3\Omega$ ,  $R_2 =$  $0.3\Omega$ ,  $X_1 = 0.41 \Omega$ ,  $X_2 = 0.41\Omega$ . neglect shunt branch in the equivalent circuit. The starting current (in Ampere) for this motor when connected to an 80V (line), 20Hz, 3-phase, AC source is

### [GATE - 2017]

4. A 3-Phase, 4-pole, 400V, 50Hz squirrel cage induction motor is operating at a slip of 0.02. The speed of the rotor flux in mechanical rad/sec. Sensed by a stationary observer, is closest to

	[GATE - 2017]
(a) 1500	(b) 1470
(c) 157	(d) 154

5. The starting line current of a 415 V, 3-phase delta connected induction motor is 120A, when the rated voltage is applied to its stator winding. The starting line current at a reduced voltage of 110V, in ampere, is

[GATE - 2016]

**1.** A 4 pole induction machine is working as an **6.** A 8-pole, 3-phase, 50 Hz induction motor is of the rotor current of the motor in Hz is

### [GATE - 2016]

7. A 3-Phase, 50 Hz, six pole induction motor has a rotor resistance of  $0.1\Omega$  and reactance of  $0.92\Omega$ . Neglect the voltage drop in stator and assume that the rotor resistance is constant. Given that the full load slip is 3%, the ratio of maximum torque to full load torque is

(a) 1.567	CONT.
c) 1.948	
	the second se

[GATE - 2014] (b) 1.712 (d) 2.134

8. A three – phase, 4 pole, self exited induction generator is feeding power to a load at a frequency  $f_1$ . If the load is partially removed, the frequency becomes  $f_2$ . If the speed of the generator is maintained at 1500 rpm in both the cases, then

[GATE - 2014]

(a)  $f_1, f_2 >: 50$  Hz and  $f_1 > f_2$ (b)  $f_1 < 50$  Hz and  $f_2 > 50$  Hz (c)  $f_1, f_2 < 50$  Hz and  $f_2 > f_1$ (d)  $f_1 > 50$  Hz and  $f_2 < 50$  Hz

9. In a synchronous machine, hunting is predominantly damped by [GATE - 2014]

(a) Mechanical losses in the rotor (b) Iron losses in the rotor (c) Copper losses in the stator

(d) Copper losses in the rotor

**10.** Leakage flux in an induction motor is

[GATE - 2013]

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(a) Flux that leaks through the machine (b)Flux that links both stator and rotor windings (c)Flux that links none of the windings (d)Flux that links the stator winding or the rotor winding but not both

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Sol.1. (c) Given parameters of star -connected SCIM at Supply frequency  $(f_1) = 60$ Hz & Pole = 4 60Hz are :.  $N_s = \frac{120f}{P} = \frac{120 \times 60}{4} = 1800 rpm$  $r_1 = 0.3\Omega$ ,  $r_2 = 0.3 \Omega$  $X_1 = 0.41\Omega, \quad X_2 = 0.41 \Omega$ Now, if frequency changed to 20Hz, leakage Rotor frequency  $(f_2) = 5hz$ reactance magnitude will change. We know tht  $f_2 = sf_1$ :  $X_{1(\text{new})} = \frac{20}{60}(0.41) = 0.136\Omega$  $5 = (s) (60) \implies 0.0833$ But in induction generator, slip is a negative value  $\therefore X_{2(\text{new})} = \frac{20}{60}(0.41) = 0.136\Omega$  $\Rightarrow -0.0833 = \frac{1800 - N_r}{1800}$ j0.136Ω 0.3Ω j0.136Ω 00000  $\Rightarrow$  N<sub>r</sub> = 1950 rpm Sol.2. (0.8083)  $|V_s| = 17.87 \text{ kV}$  $|V_r| = 17.32 \text{ kV}$  $\frac{80/\sqrt{3}}{\sqrt{(0.3+0.3)^2+(0.136+0+36)^2}}$  $R = 0.25\Omega$  $X_L = 3.925 \ \Omega$  $Z = \sqrt{0.25^2 + 3.925^2}$ = 70.19A  $= 3.933 \Omega$ Sol.4. (c)  $P_{\rm r} = \frac{17.87 \times 17.32}{3.933} \cos(\theta - \delta) - \frac{0.25(17.32)^2}{3.933^2}$ A  $3-\phi$ , 4 pole, 50Hz squirrel cage induction motor operating at a slip of 0.02  $3 = \frac{17.87 \times 17.32}{3.933} \cos(\theta - \delta) - \frac{0.25(17.32)^2}{3.933^2}$ Synchronous speed =  $\frac{120F}{P}$  rpm  $\cos(\theta - \delta) = 0.0997$  $=\frac{120\times50}{4}=1500$ rpm  $(\theta - \delta) = 84.276^{\circ}$  $Q_{r} = \frac{|V_{s}|V_{r}|}{|Z|} \sin(\theta - 8) - \frac{X|V_{r}|^{2}}{|Z|^{2}}$  $\therefore$  rotor speed =  $(1 - s)N_s$ =(1-0.02)(1500)= 1470 rpm $=\frac{1787\times17.32}{3.933}\sin(84.276)-\frac{3.925\times17.32^2}{3.933^2}$ The speed of rotor field with respect to rotor is  $=\frac{120\times sF}{P}=30rpm$ = 2.18483 VAR  $pf = \cos \tan^{-1} \left( \frac{Q_r}{R} \right)$ The speed of rotor field with respect to stator is 1470 + 30 = 1500 rpm  $=\frac{2\pi(1500)}{60}$  rad / sec  $= \cos \tan^{-1} \left( \frac{2.18483}{1} \right)^{-1}$ = 157.07 rad/sec = 0.8083 lagSol.5. (31.8) Sol.3. (70.19 A)

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### **CHAPTER - 6** SINGLE – PHASE INDUCTION MOTOR

### **6.1 SINGLE PHASE INDUCTION MOTOR**

Alike 3 -  $\phi$  I<sub>M</sub>, 1 -  $\phi$  IM is not self starting, and operates on poor p.f., lower capacity and reduced efficiency. It has pulsating air gap field.

For starting purposes an auxiliary winding is used and hence stator of a  $1 - \phi$  IM carries two windings:

1. Main or Running winding( $S_M$ ) 2. Auxiliary or starting winding( $S_A$ )

In these motors, both main and auxiliary windings are in the circuit at the time of starting and a centrifugal switch is provided to disconnect the Auxiliary windings when rotor attains 70 to 80% of synchronous speed.

It must be noted that the space angle between  $(S_M)$  and  $(S_A)$  should be near about 90°.

### 6.2 REVOLVING FIELD THEORY OF SINGLE PHASE INDUCTION MOTOR

It is also called – double – revolving field theory of  $1 - \phi$  IM, basically states that a stationary pulsating magnetic field can be resolved into two rotating magnetic field, each of equal magnitude but rotating in opposite direction. And IM responds to each magnetic field separately, and net torque in motor is sum of the torques due to each the two magnetic fields.

Assume the stator mmf wave to be sinusoidally distributed in space and varying sinusoudally with time then,

 $\therefore$  F<sub>S</sub> = F<sub>s.max</sub> sin  $\omega$ t.cos $\alpha$ 

Where  $\cos\alpha$  is Distribution in space along the a is gap periphery Where  $\sin\omega t$  is Distribution in space alogn the a is gap periphery Where  $F_{s,max}$  is Peak maximum instantaneous alternating M.M.F

Since, 
$$\sin a \cos b = \frac{1}{2} \left[ \sin (a - b) + \sin (a + b) \right]$$
  

$$F_{s} = \frac{1}{2} F_{s.max.} \sin (\omega t - \alpha) + \frac{1}{2} F_{s.max.} \sin (\omega t + \alpha)$$

 $\Rightarrow$  This shows that the pulsating stationary mmf wave of amplitude  $F_{s.max.}$  can be resolved into, two counter rotating mmf, components of equal magnitudes as shown in figure.

At = 90°,  $F_s = F_{s.max}$  - At instant A and two components are  $= \frac{1}{2}F_{s.max}$ .

At instant B,  $\omega t = \omega t_1$  from instant A

 $F_s = F_{s.max.} \sin(\omega t_1 + 90^\circ) = F_{s.max.} \cos \omega t_1$ 

And pulsating mmf wave resolved into sinusoidal mmF. waves marked f and b, both mmf wave travelled through an angle wts to right and left respectively as :

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1. A 375 W, 230V, 50Hz, capacitor start single-phase induction motor has the following constants for the main and auxiliary windings (at starting):  $z_m = (12.50 + j15.75)\Omega$  (main winding),  $Z_a = (24.50 + j12.75)\Omega$  9auxiliary winding). Neglecting the magnetizing branch, the value of the capacitance (in  $\mu$ F) to be added in series with the auxiliary winding to obtain maximum torque at staring is \_\_\_\_.

[GATE - 2017]

**2.** In a constant V/f induction motor drive, the slip at the maximum torque

[GATE - 2016]

(a)Is directly proportional to the synchronous speed.

(b)Remains constant with respect to the synchronous speed.

(c)Has an inverse relation with the synchronous speed.

(d)Has no relation with the synchronous speed.

**3.** The direction of rotation of a single – phase capacitor run induction motor is reversed by

[GATE - 2016]

(a)Interchanging the terminals of the AC supply.

(b)Interchanging the terminals of the capacitor.(c)Interchanging the terminal of the auxiliary winding.

(d)Interchanging the terminals of both the windings.

4. In a constant V/f control of induction motor, the ratio V/f is maintained constant from 0 to base frequency, where V is the voltage applied to the motor at fundamental frequency f. Which of the following statements relating to low frequency operation of the motor is TRUE?

[GATE - 2014]

**1.** A 375 W, 230V, 50Hz, capacitor start (a)At low frequency, the stator flux increases single-phase induction motor has the following from its rated value.

(b)At low frequency, the stator flux decrease from its rated value.

(c)At low frequency, the motor saturates.

(d)At low frequency, the stator flux remains unchanged at its rated value.

**5.** A single phase induction motor is provided with capacitor and centrifugal switch in series with auxiliary winding. The switch is expected to operate at a speed of 0.7 ns, but due to malfunctioning the switch fails to operate. The torque speed characteristic of the motor is represented by





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ESE OBJ QUESTIONS 1. In a single-phase capacitor start induction 5. An 8-pole,  $1 - \phi$  induction motor is running at motor, the direction of rotation 690 rpm. What is its slip w.r.t forward and [ESE - 2016] backward fields, respectively. (a)Can be changed by reversing the main [ESE - 2007] winding terminals. (a) 0.08, 2.0(b)Cannot be changed. (b) 0.08, 1.92 (c)Is dependent on the size of the capacitor. (c) 1.92, 0.08 (d)Can be changed only in large capacitor (d) 2.0, 0.08 motors. 6. Match List-I with List-II and select the 2. For a given applied voltage and current, the correct answer using the code given below the speed of a universal motor will be lists : [ESE - 2015] List-I (a) Higher in dc excitation than in ac excitation A. General purpose split phase FHP motor (b) Higher in ac excitation than in dc excitation B. General purpose capacitor start FHP motor (c) Same in both dc and ac excitations C. Permanent split capacitor start FHP motor (d) Dangerously high in dc excitation D. Shaded pole FHP motor List-II 3. Consider the following statements : (i) Refrigerator 1. Asynchronous motor has no starting torque (ii) Hair dryers but when started it always runs at a fixed speed (iii) Unit Heaters 2. A single -- phase reluctance motor is not self (iv) Fans, blowers starting even if paths for eddy currents are [ESE - 2007] provided in the rotor **Codes:** 3. A single -phase hysteresis motor is self -(a) A-i, B-ii,C-iv, D-iii starting (b) A-i, B-ii, C-iii, D-iv Which of these statement(s) is /are correct? (c) A-iv, B-i, C-ii, D-iii [ESE - 2013] (d) A-iv, B-i, C-iii, D-ii (a) 1, 2 and 3 (b) 1 only (d) 2 and 3 only (c) 1 and 2 only 7. A 1 -  $\phi$  induction motor is running at N r.p.m. Its synchronous speed is N<sub>s</sub>. If its slip with 4. Why is centrifugal switch used in a  $1-\phi$ respect to forward field is S, what is the slip induction motor? with respect to the backward field. [ESE - 2008] [ESE - 2007] (a)To protect the motor from overloading (b) -S (a) s (b)To improve the starting performance of the (c) (1-S) (d)(2-S)motor. (c)To cut off the starting winding at an 8. Which one of the following is the type of appropriate instant. 1 -  $\phi$  induction motor having the highest power (d)To cut in the capacitor during running factor at full load? condition.

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### CHAPTER - 7 SERVO AND STEPPER MOTOR

### 7.1 INTRODUCTION

A servo system mainly consists of three basic components - a controlled device, a output sensor, a feedback system. This is an automatic closed loop control system. Here instead of controlling a device by applying the variable input signal, the device is controlled by a feedback signal generated by comparing output signal and reference input signal. When reference input signal or command signal is applied to the system, it is compared with output reference signal of the system produced by output sensor, and a third signal produced by a feedback system. This third signal acts as an input signal of controlled device.

This input signal to the device presents as long as there is a logical difference between reference input signal and the output signal of the system. After the device achieves its desired output, there will be no longer the logical difference between reference input signal and reference output signal of the system. Then, the third signal produced by comparing theses above said signals will not remain enough to operate the device further and to produce a further output of the system until the next reference input signal or command signal is applied to the system. Hence, the primary task of a servomechanism is to maintain the output of a system at the desired value in the presence of disturbances.

### 7.1.1 Working Principle of Servo Motor

A servo motor is basically a DC motor(in some special cases it is AC motor) along with some other special purpose components that make a DC motor a servo. In a servo unit, you will find a small DC motor, a potentiometer, gear arrangement and an intelligent circuitry. The intelligent circuitry along with the potentiometer makes the servo to rotate according to our wishes. As we know, a small DC motor will rotate with high speed but the torque generated by its rotation will not be enough to move even a light load. This is where the gear system inside a servomechanism comes into the picture. The gear mechanism will take high input speed of the motor (fast) and at the output, we will get an output speed which is slower than original input speed but more practical and widely applicable.

Say at initial position of servo motor shaft, the position of the potentiometer knob is such that there is no electrical signal generated at the output port of the potentiometer. This output port of the potentiometer is connected with one of the input terminals of the error detector amplifier. Now an electrical signal is given to another input terminal of the error detector amplifier. Now difference between these two signals, one comes from potentiometer and another comes from external source, will be amplified in the error detector amplifier and feeds the DC motor. This amplified error signal acts as the input power of the DC motor and the motor starts rotating in desired direction. As the motor shaft progresses the potentiometer knob also rotates as it is coupled with motor shaft with help of gear arrangement. As the position of the potentiometer knob changes there will be an electrical signal produced at the potentiometer port. As the angular position of the potentiometer knob progresses the output or feedback signal increases. After desired angular position of motor shaft the potentiometer knob is reaches at such position the electrical signal generated in the potentiometer becomes same as of external electrical signal given to amplifier. At this condition, there will be no output signal from the amplifier to the motor input

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**GATE QUESTIONS** 1. In a steeper motor, the detent torque means [GATE - 2004] [GATE - 2009] (a) Detent torque (b) Pull in torque (a) Minimum of the static torque with the phase (c) Pull- out torque (d) Holding torque winding excited 4. The following motor definitely has a (b) Maximum of the static torque with the phase permanent magnet rotor winding excited (c) Minimum of the static torque with the phase [GATE - 2004] winding unexcited (a) DC commulator motor (d) Maximum of the static torque with the phase (b) Brushless dc motor winding unexcited (c) Stepper motor (d) Reluctance motor 2. A three-phase, three stack, variable reluctance step motor has 20 poles on each rotor 5. For a 1.8°, 2-phase bipolar stepper motor, and stator stack. The step angle of this motor is the stepping rate is 100 steps /second. The [GATE - 2007] rotational speed of the motor in rpm is (b) 6° (a) 3° [GATE - 2004] (a) 15 (d) 18° (b) 30 (c) 9° (c) 60(d) 90 3. For a given stepper motor, the following torque has the highest numerical value

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